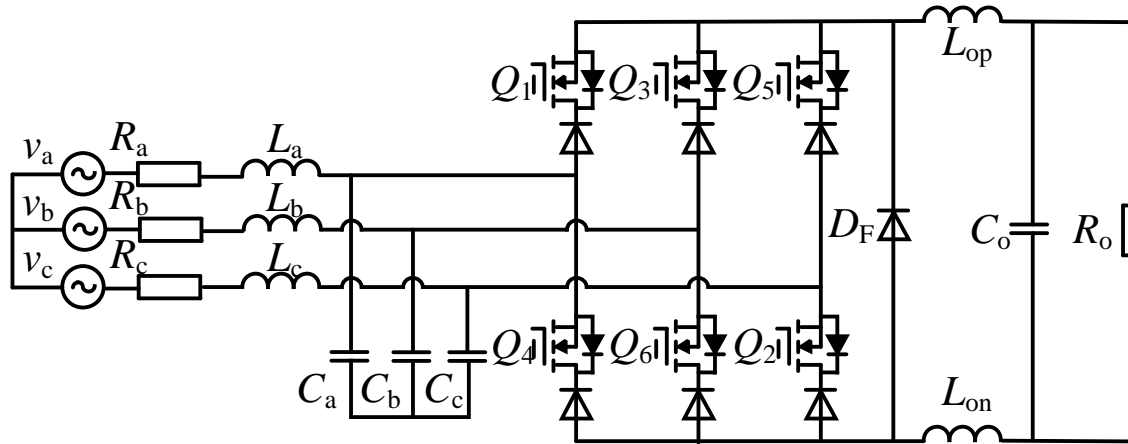


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Analysis of Input Current Distortion in Three-phase Current Source PWM Rectifier



Binghui Li, Sichuan University



Six-switch Current source rectifier



hybrid vehicle charging



new energy



telecom application

Modulation strategy

- Selective Harmonics Elimination (SHE)
 - ✓ reduction of low-order harmonics in the AC current
 - ✗ not suitable for **dynamic performance** and requires pre-computation leading to **more computational complexity**
- Sinusoidal Pulse Width Modulation (SPWM)
 - ✓ Low harmonic content in the output current and suitable for various PWM rectifier topologies
 - ✗ Difficult to implement in digital control and may result in higher switching losses
- The Space Vector Pulse Width Modulation (SVPWM)
 - ✓ More efficient utilization of DC bus voltage
 - ✓ Easy to implement and control

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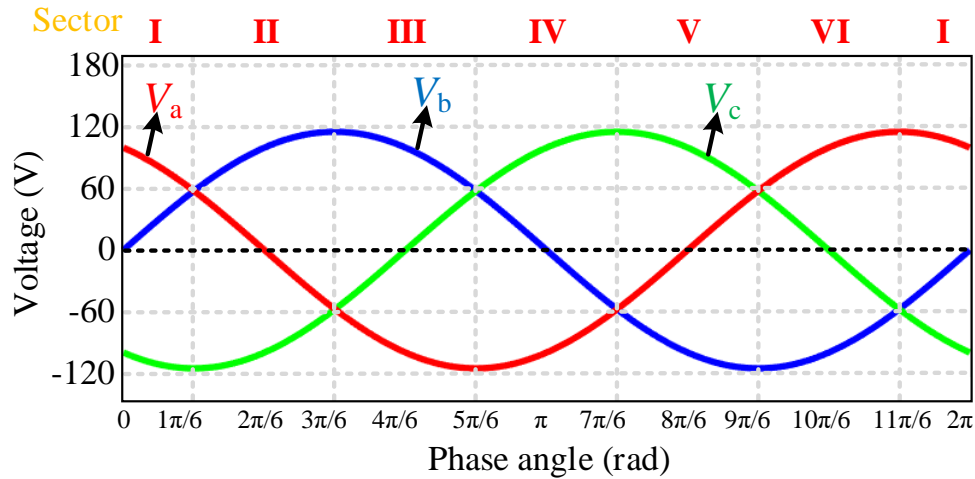
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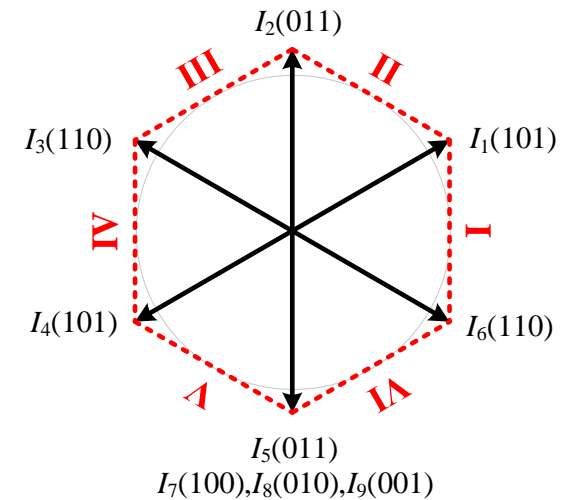
SVPWM enjoys **widespread applications**

The Space Vector Pulse Width modulation (Traditional 6-sector)

- ✓ More **efficient** utilization of DC bus voltage
- ✓ **Easy** to implement and control

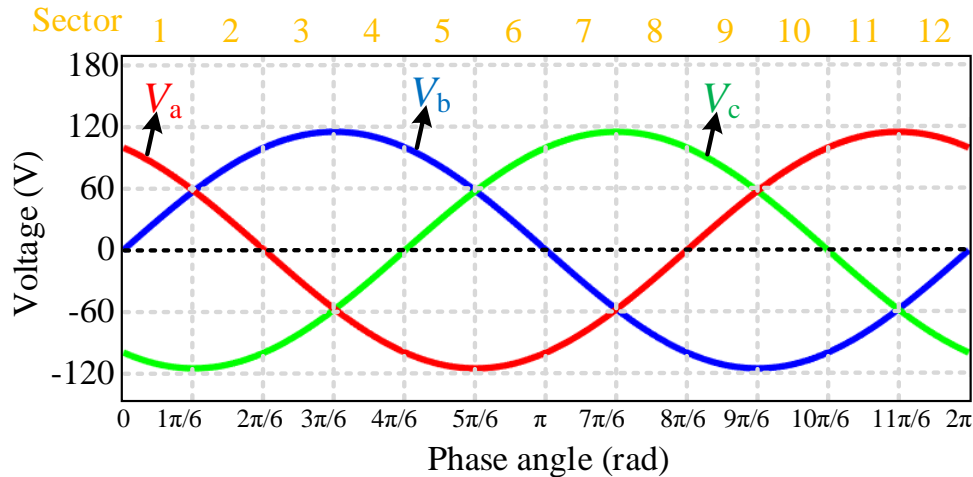


Sector division for 6-sector SVPWM in input voltage

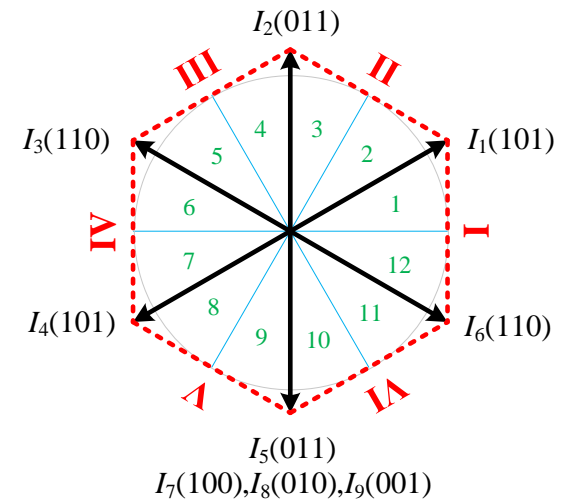


Sector division in space vector plane

- The Space Vector Pulse Width Modulation (12-sector)
 - ✓ Lower **switching losses**
 - ✓ **Reduce** inductance current ripple



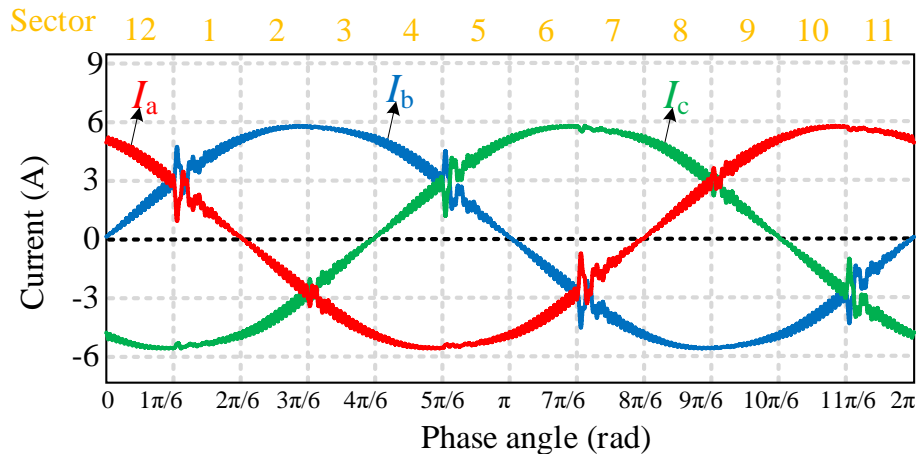
Sector division for 6-sector SVPWM in input voltage



Sector division in space vector plane

12-sector modulation exhibits **superior performance**

Hardware factors
Modulation factors



Input current waveforms

- Affect the input current harmonics [1]
- Reduce the efficiency of the rectifier [1]
- Exerts influence on the stability of the system [2]

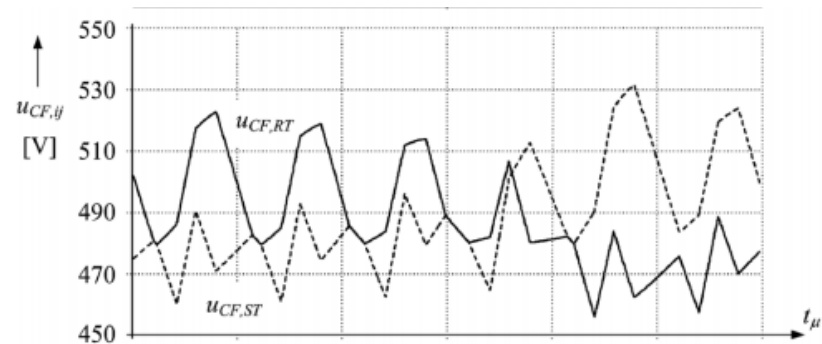
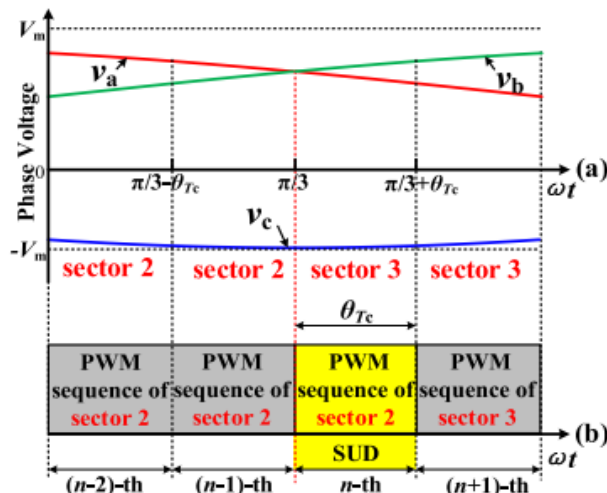
[1] T. Nussbaumer and J. W. Kolar, "Improving mains current quality for three-phase three-switch buck-type pwm rectifiers," IEEE Transactions on Power Electronics, vol. 21, DOI 10.1109/TPEL.2006.876856, no. 4, pp. 967-973, 2006.

[2] L. Schrittwieser, J. W. Kolar, and T. B. Soeiro, "Novel swiss rectifier modulation scheme preventing input current distortions at sector boundaries," IEEE Transactions on Power Electronics, vol. 32, DOI 10.1109/TPEL.2016.2609935, no. 7, pp. 5771-5785, 2017.

Hardware factors

Modulation factors

- Time delays of digital control [3]
- Sliding intersections of the input filter capacitor voltages [4]

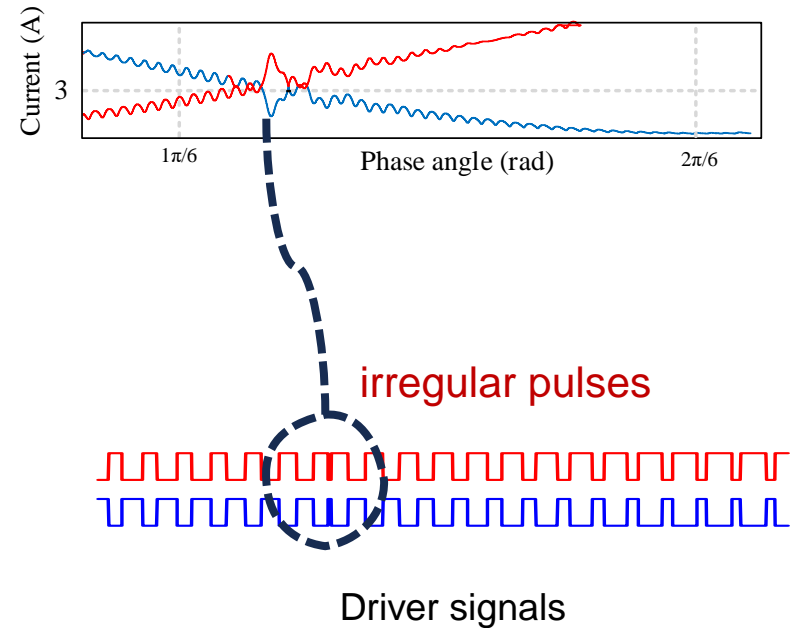
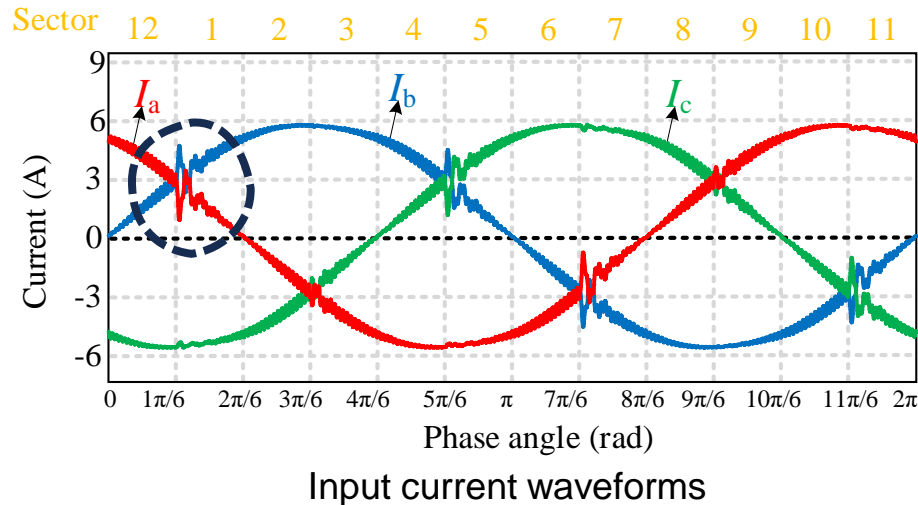


Hardware-induced distortions **effectively suppressed**

[3] Q. Chen, J. Xu, Z. Tao, H. Ma and C. Chen, "Analysis of Sector Update Delay and Its Effect on Digital Control Three-Phase Six-Switch Buck PFC Converters With Wide AC Input Frequency," in IEEE Transactions on Power Electronics, vol. 36, no. 1, pp. 931-946, Jan. 2021, doi: 10.1109/TPEL.2020.2999360.

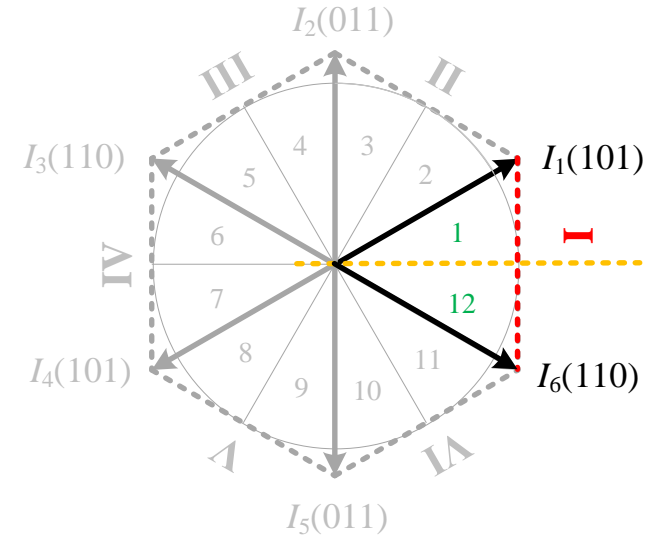
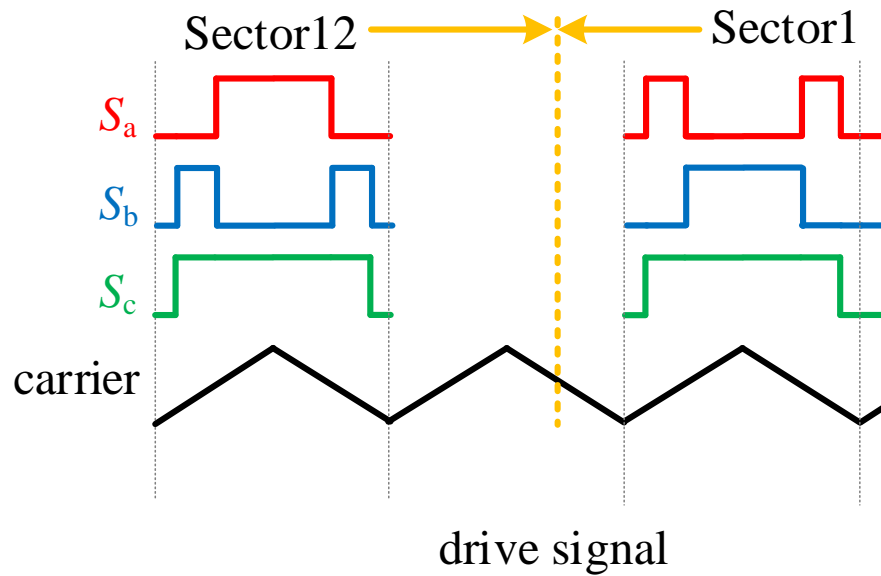
[4] T. Nussbaumer and J. W. Kolar, "Improving mains current quality for three-phase three-switch buck-type pwm rectifiers," IEEE Transactions on Power Electronics, vol. 21, DOI 10.1109/TPEL.2006.876856, no. 4, pp. 967-973, 2006.

Hardware factors
Modulation factors

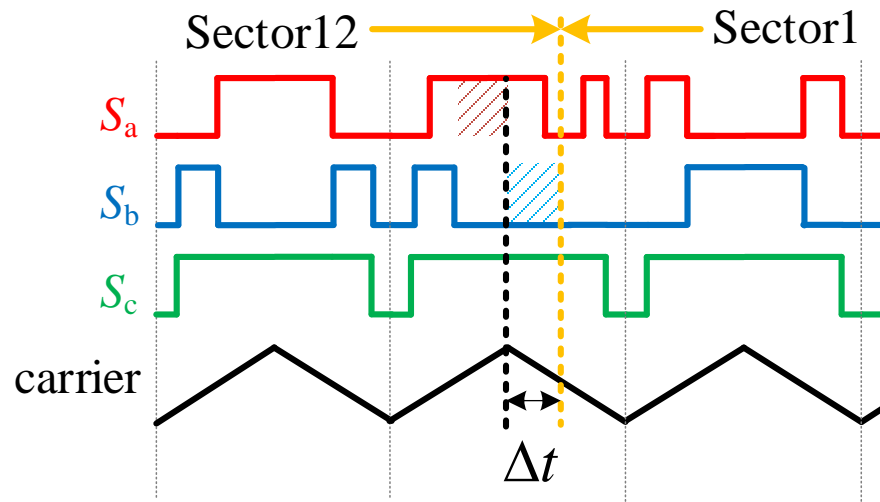


The origin of irregular pulses **remains undetermined**

[5] M. I. Haq, A. H. Hanan, A. Qadeer, B. Salimov, M. I. Younas, and I. M. Talha, "Design and implementation of an efficient single stage three phase ac-dc buck converter for hybrid vehicle charging," in 2020 IEEE 4th Conference on Energy Internet and Energy System Integration (EI2), DOI 10.1109/EI250167.2020.9346944, pp. 2930–2935, 2020.



Duty cycles **uniform** near sector boundary

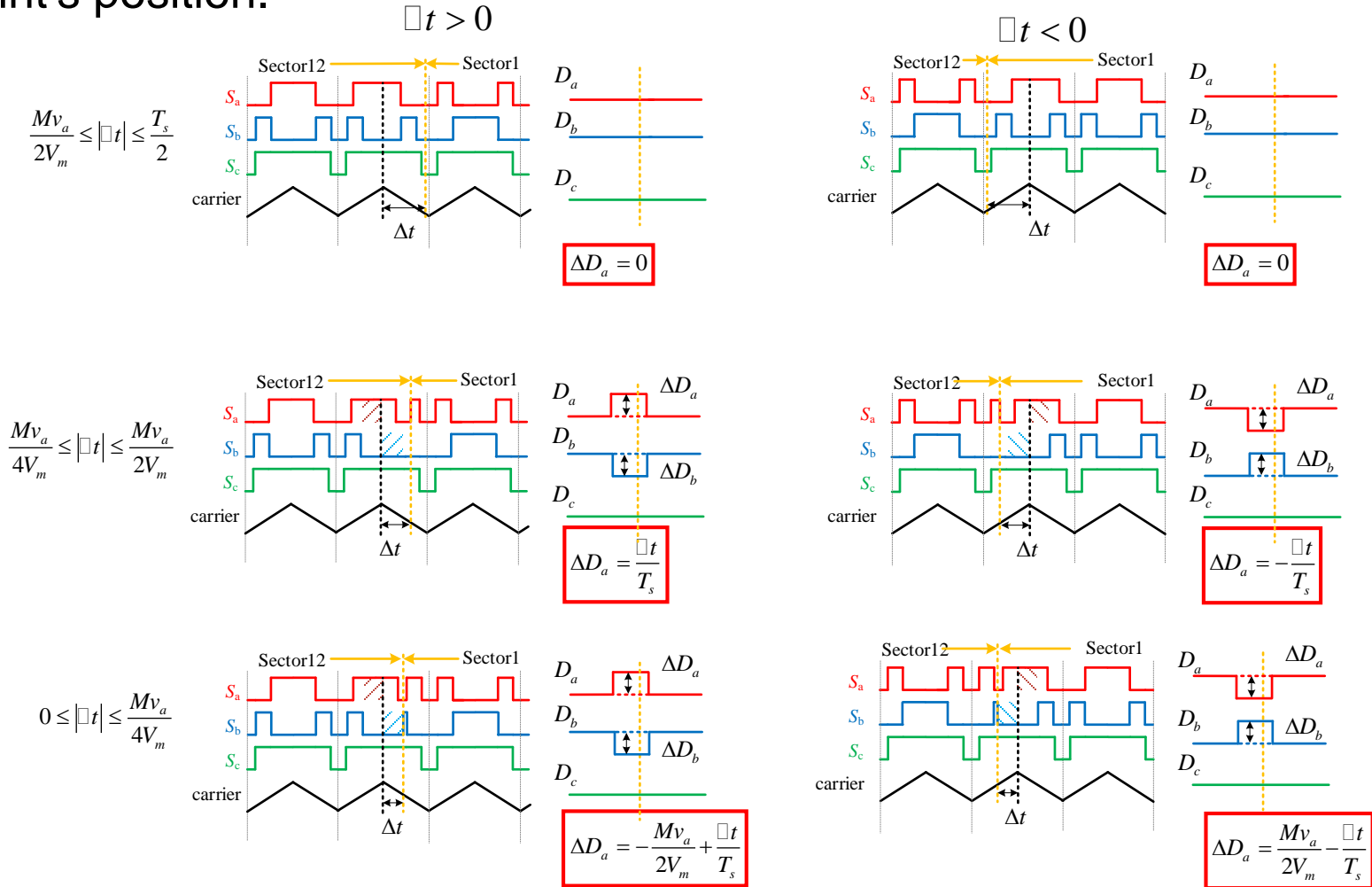


$$\Delta D_a = \frac{\Delta t}{T_s}$$

Duty cycles **change abruptly** at sector boundary

Duty cycle abrupt variation

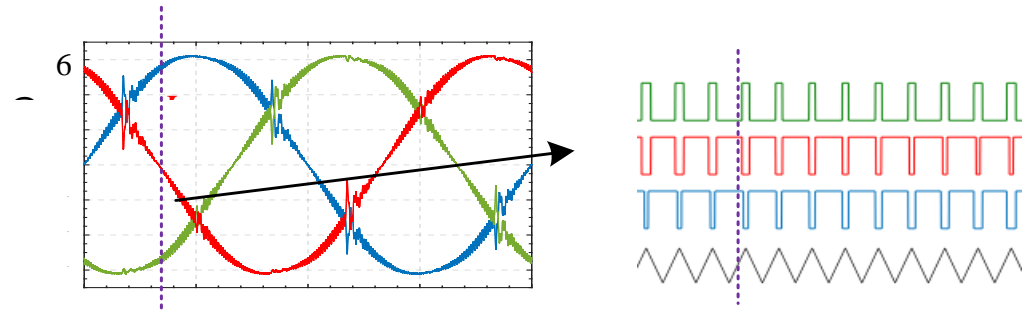
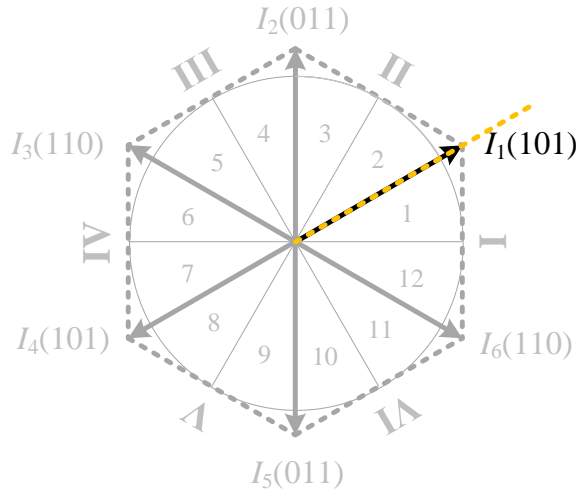
The variation in duty cycle is depending on the sector switching point's position.



$$\Delta D_a = \begin{cases} 0 & -\frac{T_s}{2} \leq \Delta t \leq -\frac{Mv_a}{2V_m} \\ -\frac{Mv_a}{2V_m} + \frac{\Delta t}{T_s} & -\frac{Mv_a}{2V_m} \leq \Delta t \leq -\frac{Mv_a}{4V_m} \\ -\frac{\Delta t}{T_s} & -\frac{Mv_a}{4V_m} \leq \Delta t \leq 0 \\ \frac{\Delta t}{T_s} & 0 \leq \Delta t \leq \frac{Mv_a}{4V_m} \\ \frac{Mv_a}{2V_m} - \frac{\Delta t}{T_s} & \frac{Mv_a}{4V_m} \leq \Delta t \leq \frac{Mv_a}{2V_m} \\ 0 & \frac{Mv_a}{2V_m} \leq \Delta t \leq \frac{T_s}{2} \end{cases}$$

- Applying compensation to irregular pulses can mitigate current distortion
- Increasing the switching frequency can mitigate current distortion [6]

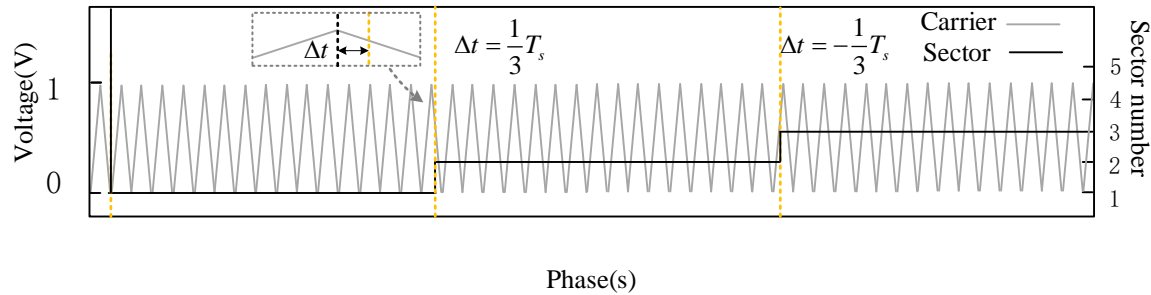
[6] M. I. Haq, A. H. Hanan, A. Qadeer, B. Salimov, M. I. Younas, and I. M. Talha, "Design and implementation of an efficient single stage three phase ac-dc buck converter for hybrid vehicle charging," in 2020 IEEE 4th Conference on Energy Internet and Energy System Integration (EI2), DOI 10.1109/EI250167.2020.9346944, pp. 2930–2935, 2020.



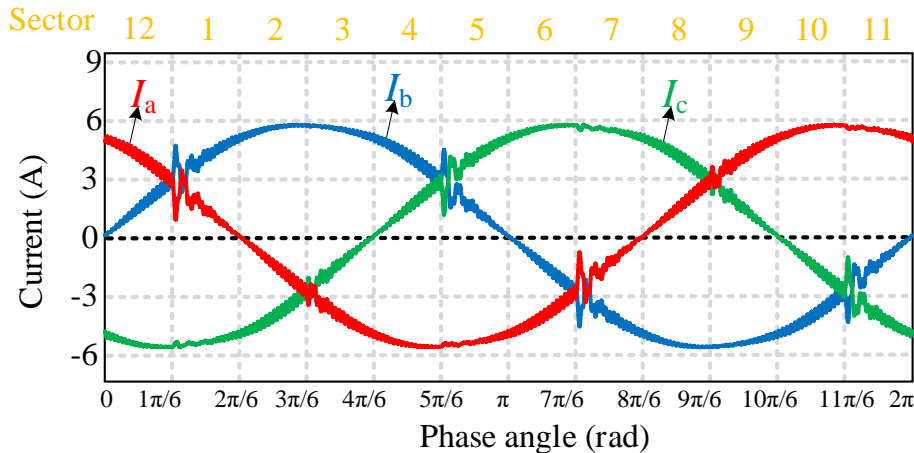
Only one effective vector is applied

No irregular pulses

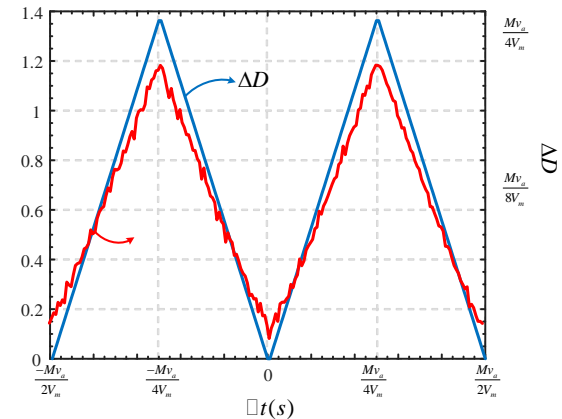
Transit smoothly in large sector switches



When the carrier frequency and position are fixed Δt exhibits **periodic variation** at each sector boundary



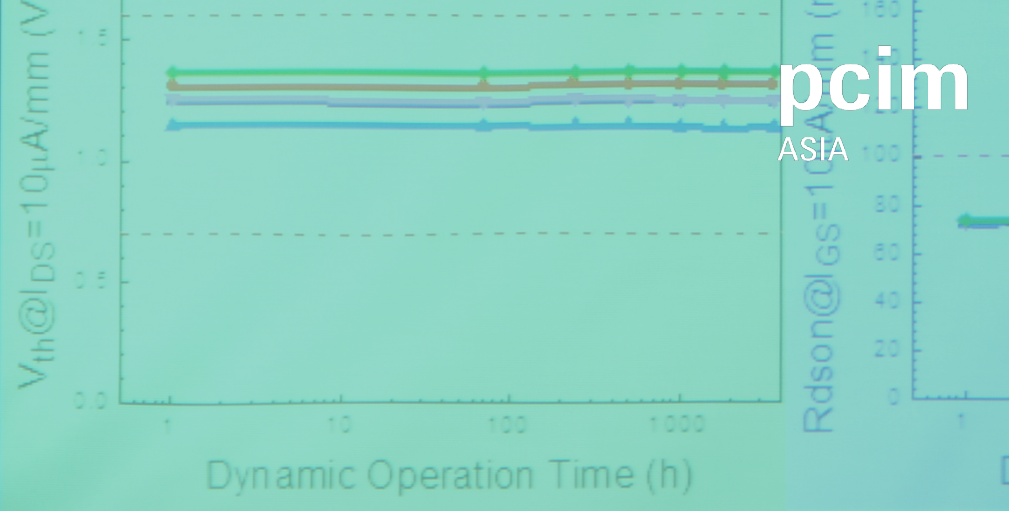
The degree of current distortion demonstrates **corresponding periodic variation**



Relationship between the degree of current distortion duty cycle variation, and Δt

The simulation results **validate** the theoretical analysis

- Investigates **the cause of current distortion**, which arises from irregular pulses (resulting from the difference between carrier and sector switching points' positions)
- Explains the **periodic variation** in the degree of current distortion
- Provides an explanation for why current distortion occurs **only when transitioning from even to odd sectors**



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 University



Thank you

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